

IMPEDANCE MATCHED LOW NOISE AMPLIFIER

FIELD OF THE INVENTION

[001] The present invention relates to impedance matched low noise amplifiers and, more particularly, to an impedance matched low noise amplifier using feedback to achieve low noise and impedance matching.

BACKGROUND OF THE INVENTION

[002] The present invention achieves advantages as an impedance matched low noise amplifier. Prior designs that provide impedance matching while maintaining low noise are based on a low noise high impedance amplifier with negative feedback to provide a matched-impedance at the input. Such designs work adequately but suffer from noise boosting that is dependent on the parasitic input capacitance and open loop gain of the high impedance amplifier. The present invention uses a low impedance low noise amplifier and uses positive gm feedback to boost the input impedance to a desired matched value. The net result is an impedance-matched amplifier with noise performance similar to the low impedance amplifier before feedback is applied.

SUMMARY OF THE INVENTION

[003] In one embodiment of the present invention, an impedance matched low noise amplifier circuit comprises a serially coupled first resistor and first transistor, a serially coupled second resistor and second transistor, a resistive sensor coupled to the first transistor and the second transistor, wherein the first resistor and the second resistor are coupled, and a transconductance feedback block coupled to the resistive sensor and to the serially coupled resistors and transistors.

[004] In another embodiment of the present invention, a method for increasing an input impedance of an amplifier comprises determining an input impedance at each of

a first transistor and a second transistor, matching the input impedance to an impedance of an interconnect between the inputs of the first transistor and the second transistor, conducting data signals from a resistive sensor coupled to the first transistor and the second transistor to the inputs, and decreasing current to the transistors, by a transconductance feedback block coupled to the resistive sensor and to the transistors, by an amount dependant on the voltage between the transistors.

BRIEF DESCRIPTION OF THE DRAWINGS

[005] Fig. 1 illustrates an impedance matched low noise amplifier in accordance with an exemplary embodiment of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

[006] CIRCUIT DESCRIPTION

[007] Referring now to Fig. 1, an impedance matched low noise amplifier circuit 10 consists of low noise transistors **Q0** and **Q1** (which may be MOS or Bipolar transistors), load resistors **RL1** and **RL2**, resistive sensor **RMR**, and transconductance feedback block **GM**.

[008] The base of transistor **Q0** is connected to supply voltage **VMRP**. Load resistor **RL1** is connected between the collector of **Q0** and supply voltage **VREF**. The emitter of transistor **Q0** is connected to one end of resistive sensor **RMR**. The other end of resistive sensor **RMR** is connected to the emitter of transistor **Q1**. The base of transistor **Q1** is connected to supply voltage **VMRP**. Load resistor **RL2** is connected between the collector of **Q1** and supply voltage **VREF**. The common node of resistor **RL2** and the collector of transistor **Q1** is connected to the second input of the transconductance feedback block **GM**. The common node of resistor **RL1** and the collector of transistor **Q0** is connected to first input of the transconductance feedback block **GM**. The first output of the transconductance feedback block **GM** is connected to the common node of the emitter of transistor **Q0** and the resistive sensor **RMR**. The second output of the transconductance feedback block **GM** is connected to the common node of the emitter of transistor **Q1** and the resistive sensor **RMR**.

[009] CIRCUIT OPERATION

[010] In the low noise amplifier circuit 10, transistor **Q0** and transistor **Q1** perform as common-base amplifiers. The input of each common-base amplifier is at its transistor's emitter. The output of each common-base amplifier is at its transistor's collector. In order for the common-base amplifiers at **Q0** and **Q1** to have the best noise performance, a low input impedance results. For a common-base amplifier, the input impedance will decrease as the emitter current is increased. Increasing the emitter

current reduces the noise generated by the amplifier. As such, low-noise common-base amplifiers result in low impedance inputs. It is noted that if MOS transistors were used in the circuit 10, they would perform as common-gate amplifiers. In such a situation, the input of each common-gate amplifier would be at its transistor's source, and the output of each common-gate amplifier would be at its transistor's drain.

[011] For the circuit 10, the input impedance of each common-base amplifier is determined by the bias current supplied to the emitter of each of transistors **Q0** and **Q1**. The circuit to supply this bias current to the emitters of transistor **Q0** and transistor **Q1** is not shown.

[012] The low input impedance at each of the common-base amplifiers at **Q0** and **Q1** may not provide a good match to the impedance of the interconnect between the resistive sensor **RMR** and the inputs of the common-base amplifiers. It is desirable to have the input impedance of the common-base amplifiers **Q0** and **Q1** be matched to the impedance of the interconnect between these amplifier inputs in order for data signals from the resistive sensor **RMR** to be conducted to the inputs of the amplifiers with the best signal quality. When data is being sensed by the resistive sensor **RMR**, this data will be seen as a positive or negative voltage difference across **RMR**. It is this voltage across resistive sensor **RMR** that represents data being read from a hard disk in a disk drive storage device. This voltage across **RMR** will appear at the input of each common-base amplifier at **Q0** and **Q1**. When the voltage across resistive sensor **RMR** changes, this voltage change will be amplified by the common-base amplifiers and will cause a change in the output voltage at the collector of each of transistors **Q0** and **Q1**. Thus, the voltage between the collectors of **Q0** and **Q1** will change in response to the change in voltage across the resistive sensor **RMR**.

[013] The transconductance feedback block **GM** will act to reduce the AC current to the emitters of **Q0** and **Q1** by an amount that is dependant on the AC voltage between the collectors of **Q0** and **Q1** and the gain of the transconductance feedback block **GM**. This decrease in the emitter AC current will cause an increase in the input

impedance of the common-base amplifiers at Q0 and Q1. Thus, the input impedance of the common-base amplifiers at Q0 and Q1 will be increased by an amount that is proportional to the voltage between the input connections of the transconductance feedback block GM. The noise behavior of the front end amplifier is only slightly increased by the AC feedback. Thus, low-noise can be achieved by choosing a high bias current and the input impedance of the amplifier can be raised with positive gm feedback. This results in near independent control of noise behavior and input impedance for the amplifier.

[014] CIRCUIT SUMMARY

[015] The impedance matched low noise amplifier circuit 10 of the present invention utilizes a common base amplifier consisting of Q0 and Q1 and load resistors RL1 and RL2 with gm feedback to achieve low noise and impedance matching. The gm feedback boosts the low impedance at Q0 and Q1 emitters to a level that is adequate for impedance matching the amplifier front end to the interconnect that leads to the RMR sensor. The impedance at the emitters of Q0 and Q1 before feedback is applied is driven low to achieve low noise. This is achieved by increasing the bias current of Q0 and Q1 that in turn reduces the impedance. The impedance reduction from an AC signal standpoint is not desirable if the impedance is driven lower than the desired matching impedance. Typical impedance for low noise is on the order of 15 ohms differential. Desired impedance for matching is on the order of 70 ohms differential. The gm feedback allows the amplifier to run at a noise impedance of 15 while AC impedance can be tuned up to match the interconnect.

[016] Although an exemplary embodiment of the present invention has been illustrated in the accompanied drawings and described in the foregoing detailed description, it will be understood that the invention is not limited to the embodiments disclosed, but is capable of numerous rearrangements, modifications, and substitutions without departing from the spirit of the invention as set forth and defined by the following claims.